

DEFENSE THREAT REDUCTION AGENCY
NUCLEAR TEST PERSONNEL REVIEW PROGRAM
RADIATION DOSE ASSESSMENT

STANDARD METHOD

UA01 – Dose Uncertainty and Upper Bound Determinations

Revision 1.3a

Key to SOP ID Codes

*RA (Radiation Assessment - SOP)
ED (External Dose - Standard Methods)
ID (Internal Dose - Standard Methods)
UA (Uncertainty Analysis - Standard Methods)*

Table of Contents

Table of Contents.....	3
List of Tables	4
1 Purpose/Summary	5
2 Scope.....	5
3 Responsibilities.....	5
4 Definitions.....	5
5 Method Descriptions.....	5
5.1 Deterministic Method	6
5.1.1 Uncertainties and Upper Bounds in External Dose	6
5.1.2 Uncertainties and Upper Bounds in Internal Dose	12
5.1.3 Uncertainties and Upper Bounds in Skin Dose.....	14
5.2 Probabilistic Method.....	17
5.2.1 Uncertainties in External Dose	18
5.2.2 Uncertainties in Internal Dose Models	24
5.2.3 Treatment of Correlations	28
6 Data and Input.....	28
7 Referenced SOPs from this Manual.....	28
8 Reference Materials	28
Attachment 1 Sample Uncertainty Calculations.....	31
Attachment 2 Implementation of Probability Density Functions in Mathcad.....	34

List of Tables

Table 1. Sample Output from FBDOSE Program	10
Table 2. Proposed Ranges of Uncertainty Factors for Estimating Point Values Using Measured Intensities and Iso-Intensity Contour Maps	23

Standard Method

UA01 – Dose Uncertainty and Upper Bound Determinations

1 Purpose/Summary

Standard Method (SM) UA01, *Dose Uncertainty and Upper Bound Determinations*, provides general technical and computational methods for assessing the upper bounds for external (gamma and neutron), internal, and skin doses for individuals in the Nuclear Test Personnel Review (NTPR) Program according to the procedures specified in SOP RA01. The upper-bound dose represents the minimum dose that was received by less than five percent of the population of participants who were exposed under similar conditions. That is, 95 percent of all the veterans exposed under similar conditions received a dose smaller than the upper-bound dose. As such, the upper-bound dose is the 95th percentile of the dose distribution.

2 Scope

This standard method provides technical guidance for calculating the upper bound external, internal, and skin doses for personnel resulting from exposure to a nuclear detonation and to the resulting radioactive material, including both fallout and activated sources. This standard method is used in conjunction with other standard methods for assessing radiation exposures in accordance with the requirements of Title 32, Code of Federal Regulations, Part 218, *Guidance for the Determination and Reporting of Nuclear Radiation Dose for DoD Participants in the Atmospheric Nuclear Test Program*.

3 Responsibilities

Qualified radiation dose analysis staff members use these methods and associated tools for assessing the upper bound radiation doses for exposed individuals.

4 Definitions

- Uncertainty factor: The ratio of the upper bound dose to the best estimate dose.
- Upper bound: A reconstructed dose that has a 95-percent probability of being equal to or greater than the actual dose. This is set equivalent to the 95th percentile of a probabilistically determined dose distribution.

5 Method Descriptions

The NTPR Program uses two methods—deterministic and probabilistic—for estimating dose uncertainties with the objective of producing an upper bound dose that represents at least the 95th percentile of the dose to the exposed population. That is, that the estimated dose will be greater than the dose received by 95 percent of the veterans in similar

conditions. The deterministic method is based on high-sided estimates of key parameters and fixed uncertainty factors that are thought to produce a credible upper bound and are considered “veteran friendly” in the absence of full consideration of uncertainties. The probabilistic method uses Monte Carlo simulations to provide a full analysis of uncertainties. The Monte Carlo simulations consist of randomly sampling values of the input parameters from their credible assigned probability distributions; those values are input to the dose models to build an output distribution of dose, whose summary statistics are calculated. Such distributions account for both inaccuracy and spatial and temporal variability of input parameters to dose models. Procedures are available (SOP RA01) to select the method that produces a credible upper bound dose with the best use of time and resources. The following two sections discuss the deterministic and the probabilistic methods.

5.1 Deterministic Method

This section describes the methods used to calculate the upper bound doses of deterministically reconstructed mean doses and film badge doses. The following subsections discuss the uncertainties and upper bound doses associated with neutron dose, reconstructed external gamma dose, doses from film badges, reconstructed internal doses, and skin doses.

5.1.1 Uncertainties and Upper Bounds in External Dose

The uncertainties in external dose are treated as if they are normally distributed when combining uncertainties (even if they are more appropriately characterized by a different distribution), and are combined using statistical methods appropriate for normally distributed data. External gamma and neutron doses, if they are accrued from different locations or different sources, are assumed to be statistically independent. Doses from multiple detonations accrued while aboard a given ship or on a particular residence island during a single operation, or during multiple operations where the participant’s duties have not appreciably changed, are treated as being correlated, because the major source of uncertainty is from the assumed exposure scenario (e.g., time spent indoors versus outdoors or topside versus below deck). Because neutron doses are reported separately from external gamma doses, the statistical combination of those two doses is unnecessary.

5.1.1.1 Neutron Dose

There are few instances where participants were exposed to neutron radiation from a nuclear detonation. In those cases, rigorous assessments have been performed to determine estimates of the neutron environments created by the respective detonations. The consequences of adoption of certain recommendations about neutron dose of a committee of the National Research Council of the National Academy of Science (NRC, 2003), the contemporary best-estimate neutron equivalent doses were increased by

approximately a factor of 2, mostly due to an increase from 10 to 20 of the radiation weighting factor (previously referred to as “quality factor”) for neutrons subsequent to previous calculations of neutron dose. Uncertainties in the original neutron doses were assessed based on estimates of the uncertainties in the underlying parameters (e.g., source spectrum and intensity, flux asymmetry) and combined to generate a total uncertainty in the prompt neutron dose. Reported uncertainties have been reevaluated after NRC’s 2003 recommendations and are appropriate for current neutron dose assessments. Thus, the neutron dose uncertainty factors derived in the analysis of radiation exposure reports prepared for specific groups and ships for certain operations and shots (commonly called the “White Books”) should be multiplied by the revised best estimated neutron dose contained in Weitz and Egbert (2009) to determine the upper bounds of the neutron doses (DTRA, 2007). Specific information on neutron equivalent doses and their uncertainties is provided for specific operations in Appendices A–C.

5.1.1.2 Reconstructed External Gamma Dose

Under current guidance for deterministic assessments (DTRA, 2007), whole body external gamma doses from initial gamma radiation are assessed an uncertainty factor based on the uncertainty as determined by gamma transport modeling or measurement for participants who were not wearing film badges. The estimates of mean initial gamma dose and the uncertainty factors can be found in the analysis of radiation exposure reports prepared for specific groups and ships for certain operations and shot (“White Books”). The initial gamma uncertainty factors should be multiplied by the revised best estimates for initial gamma doses contained in Weitz and Egbert (2009) to determine the upper bounds of the initial gamma doses (DTRA, 2007). Specific information on initial gamma doses and their uncertainties is provided for specific operations in Appendices A–C.

Whole body external gamma doses from residual radiation exposure (e.g., fallout, and neutron-activated soil) are assigned a nominal uncertainty factor of 3. Higher (or lower) factors should be used if demonstrably justified by a greater (smaller) uncertainty in one or more aspects of the scenario such as assigning an uncertainty to a film badge result (SAIC, 2006).

Upper Bound for Reconstructed Gamma Dose

For a reconstructed deterministic whole body gamma dose, the upper bound is given by:

$$UB_{\gamma} = UF_{ext} D_{\gamma} \quad (1)$$

where

UB_{γ} = The upper bound dose (rem)
 D_{γ} = Whole body external gamma dose (rem)

UF_{ext} = Uncertainty factor associated with reconstructed whole body external gamma dose, assumed to be 3 in deterministic dose assessments

The upper bound uncertainty factor for whole body external gamma dose is set to 3 in deterministic models as recommended in the NTPR policy and guidance manual (DTRA, 2007).

Total Dose, Uncertainty, and Upper Bound for Reconstructed Whole Body External Gamma Dose

For n reconstructed deterministic whole body external gamma dose components, the total whole body external gamma dose, dose component uncertainty, and the upper bound dose are given by:

$$D_{\gamma} = \sum_{i=1}^n D_{\gamma,i} \tag{2}$$

$$u_{\gamma,i} = D_{\gamma,i}(UF_{ext} - 1) \tag{3}$$

$$UB_{\gamma} = D_{\gamma} + \sqrt{\sum_{i=1}^n u_{\gamma,i}^2} \tag{4}$$

where

- D_{γ} = Whole body external gamma dose (rem)
- $D_{\gamma,i}$ = The i^{th} component of the total gamma dose D_{γ} (rem)
- $u_{\gamma,i}$ = The uncertainty associated with the i^{th} component of the total reconstructed gamma dose D_{γ} (rem)
- UB_{γ} = The total upper bound whole body external gamma dose (rem)

5.1.1.3 Dose from Film Badges

Uncertainties associated with film badge readings are treated differently than the uncertainties for reconstructed whole body gamma doses (DTRA, 2007). The uncertainty for film badge readings has many sources and is handled differently for individually issued, permanent or mission, dosimeters than for cohort film badges.

Uncertainties in film badge dosimetry are treated using the guidance contained in the report entitled Film Badge Dosimetry in Atmospheric Nuclear Tests (NRC, 1989). With all dose uncertainty calculations associated with film badges, the total reported mean

dose is the officially recorded film badge reading while the upper bound assessment uses the bias-corrected mean dose, which is derived from recommendations in NRC (1989). The exceptions to this general approach are for Operations BUSTER-JANGLE and TUMBLER-SNAPPER, where the bias correction is greater than the overall uncertainty and the calculated upper bound dose is less than the reported dose for a given badge. For those operations, the NTPR program considers the recorded film badge reading and the upper bound to be one and the same.

Sources of Uncertainty in Film Badge Readings

The NTPR program implements three of the four principal types of bias and uncertainty that affect film badge dosimetry results for atmospheric nuclear test participants discussed in NRC (1989). These types of bias and uncertainty are radiological, laboratory, and environmental factors. The fourth source of bias and uncertainty discussed in NRC (1989) is the conversion of film badge (FB) exposure in milliRoentgens (mR) to Deep Dose Equivalent (DDE) (USNRC, 2006) in millirem (mrem), which is the dose equivalent from penetrating radiation to soft tissue located at a depth of 10 millimeters in the body and is due to variations in geometries and size and shape of individual badge wearers. NTPR does not consider the bias caused by the FB to DDE conversion but does consider the uncertainty. (SAIC, 2006)

In addition to the types of uncertainties associated with bias in film badge results, there are several sources of inaccuracy due to film badge handling, administration, and documentation. These non-statistical categories of inaccuracy include film badge readings that are too low or too high for the exposure scenario, or inaccuracies due to film badge damage that made the film badge incapable of being properly analyzed during processing. The handling of these types of inaccuracies is explained in SM ED01.

In addition to the uncertainties associated with individual film badges, the use of cohort film badges creates additional uncertainty. The additional uncertainty is due to variations in activities and locations that would cause variation in the doses between the badge wearing member of the cohort and others in the cohort. (NRC, 2003)

Uncertainty and Upper Bound for Film Badge Readings

NTPR uses the FBDOSE program (SAIC, 2006) to estimate the component of external gamma dose, uncertainty, and upper bound dose from film badge readings. The FBDOSE manual has a detailed discussion of how to run the program, enter data, and use the output. An example of an FBDOSE output (FBDOSE.OUT) is given in Table 1. Although specific to Operation BUSTER-JANGLE, the format in the example in Table 1 is completely generic.

Table 1. Sample Output from FBDOSE Program

FILM BADGE INTERVAL	MR	MRADJ	FILM BADGE DOSE LOWER	DOSE MEAN	EQUIV UPPER	UPP90	EXPL
10 28 51 TO 10 28 51	380	380	221	332	498	466	
10 28 51 TO 10 28 51	0	0	0	0	0	0	3
10 30 51 TO 10 31 51	240	240	139	209	314	294	
11 5 51 TO 11 5 51	0	20	0	17	57	47	5
11 19 51 TO 11 19 51	100	100	52	87	145	134	
11 29 51 TO 11 29 51	140	140	77	122	192	178	
11 30 51 TO 12 2 51	320	320	186	279	419	393	
12 3 51 TO 12 3 51	190	190	109	166	252	235	
TOTALS FOR FB, FBDE: PCT)	1370	1390	903	1215	1633	(1557 @ 90	
EXPLANATION CODES: 1 = UNIT DOSIMETRY READS ZERO 2 = RECONSTRUCTED ZERO DOSE 3 = NO EXPOSURE POTENTIAL 4 = HELD AS ZERO PENDING RESEARCH TO DEFINE EXPOSURE 5 = CONVERTED TO HALF OF MDL 6 = TOTAL OF MULTIPLE FILM BADGE READINGS							

The FBDOSE variable names in the output above are defined as follows:

FILM BADGE INTERVAL – Dates of coverage for each badge as input by the user in MM DD YY format.

MR – Film badge reading (mrem) for each badge and their total sum.

MRADJ – Film badge reading (mrem) adjusted to account for sub-MDL doses and their total sum. In Table 1, the first zero badge was treated as a “definite” zero and the second as a “soft” zero resulting in an assigned dose equal to 20 mrem, which is half of the minimum detection limit (MDL) of 40 mrem.

LOWER – Lower limit of the 95-percent confidence interval associated with each individual mean dose equivalent and total dose equivalent (mrem).

MEAN – Central estimate of dose equivalent (mrem) for each exposure and for the total dose equivalent (Bias removed).

UPPER – Upper limit of the 95-percent confidence interval associated with each individual mean dose equivalent and total dose equivalent (mrem). UPPER includes 97.5 percent of the dose distribution.

UPP90 – Upper limit of the 90-percent confidence interval, which brackets the 5th to 95th percentile, associated with each individual mean dose equivalent and total dose equivalent (mrem). This value is used for reporting the 95th percentile upper bound dose.

The analyst uses the total in the MRADJ column shown in Table 1 as the best estimate of the external gamma dose that was recorded by one or more film badges and the total of the UPP90 column as the upper bound 95th percentile dose. For external dose involving only film badge readings, upper bound dose and the uncertainty of the film badge dose are given by:

$$D_{\gamma} = FB_{\gamma} \quad (5)$$

$$UB_{FB\gamma} = FB_{UB} \quad (6)$$

$$u_{FB\gamma} = FB_{UB} - FB_{MEAN} \quad (7)$$

where

FB_{γ}	=	The total dose from all film badge dosimetry taken from the total of the MRADJ column of the FBDOSE output and converted to rem
FB_{UB}	=	The upper bound for all film badge dosimetry taken from the UPP90 column of the FBDOSE output and converted to rem
FB_{MEAN}	=	The total mean film badge dose adjusted for bias taken from the MEAN column of the FBDOSE output and converted to rem
$UB_{FB\gamma}$	=	The upper bound whole body external gamma dose based only on film badge readings (rem)
$u_{FB\gamma}$	=	The uncertainty of the film badge gamma dose (rem)

The uncertainty associated with the total film badge dose, $u_{FB\gamma}$, is used to estimate upper bound doses involving a combination of film badge readings and reconstructed whole body external doses.

Uncertainty and Upper Bound in Cohort Film Badge Readings

Because cohort badges have a greater degree of uncertainty than individually issued permanent or mission film badges, the FBDOSE-based method of uncertainty analysis should not be used (Kocher, 2004). When using cohort film badges, the mean dose should be calculated using the FBDOSE program the same as above. However, when an external gamma dose is estimated based on the results from one or more film badges worn by other members of a participant's exposure cohort, the external uncertainty factor (UF_{ext}) factor should be applied (See Equation 4). This uncertainty is calculated using Equation 3.

Exceptions to the use of the external uncertainty factor (UF_{ext}) to estimate the participant's external gamma upper bound dose using cohort film badge results can be justified based on knowledge of the participant's exposure scenario. If sufficient knowledge of the individual's exposure scenario is known, then the individual film badge

method of uncertainty analysis should be performed for the cohort film badge result. (Kocher, 2004)

5.1.1.4 Combined Reconstructed and Film Badge External Gamma Doses

The total gamma doses and their associated uncertainties from each of the two categories (reconstructed whole body external gamma and film badge-based) are combined assuming the dose distributions are normal (even though it is likely both tend towards being lognormal or something different entirely). This assumption simplifies the calculations required to generate an upper bound dose and does not appreciably change the result. As was stated above, what is important to remember is that, if film badges are part of the uncertainty calculation, the reported film badge dose is used for the reported mean total external gamma dose, while the bias-corrected mean dose is used with its associated uncertainty for the upper bound external gamma dose.

Estimate and Upper Bound for Reconstructed Gamma Dose and Film Badge Dose

For n reconstructed gamma dose components and film badge results, the total whole body external gamma dose and the upper bound dose are given by:

$$D_{\gamma} = \sum_{i=1}^n D_{\gamma,i} + FB_{\gamma} \quad (8)$$

$$UB_{\gamma} = \sum_{i=1}^n D_{\gamma,i} + FB_{MEAN} + \sqrt{\sum_{i=1}^n u_{\gamma,i}^2 + u_{FB\gamma}^2} \quad (9)$$

Note: The uncertainty for the reconstructed doses is given by Equation 3 and the uncertainty for film badge results is given in Equation 6.

5.1.2 Uncertainties and Upper Bounds in Internal Dose

Prior to NRC's 2003 recommendations, internal doses were reported using a single point estimate that, based on the high-sided value used for the resuspension factor and other factors, was considered to be equivalent to or greater than the 95th percentile. However, the uncertainty in the dose coefficients used to calculate those internal doses was not taken into account. Therefore, it was estimated that all previously reported (upper bound) internal doses could be low by a factor of 10 or perhaps more. For convenience, an uncertainty factor (UF_{int}) of 10 was promulgated in the DTRA's Interim Guidance for the NTPR Program (DTRA, 2003). Because the previously reported "best estimate" doses were still high-sided, it should be understood that those doses are not true means and that the uncertainty factor of 10 is in addition to the already included high-sided parameters

underlying that previously reported best estimate dose. An uncertainty factor of 1 is used for incidental ingestion since that internal dose calculation is extremely high-sided.

Internal doses, having uncertainties that are not necessarily related to the source or location of the exposure, may be combined assuming all internal component doses are fully correlated. Though it is possible that there is some degree of independence among the component doses, NTRP assumes the component doses are fully correlated (DTRA, 2007). An exception is made when combining internal doses based on mission film badges that have different issue and return dates. This exception is discussed below.

5.1.2.1 Reconstructed Internal Dose

The total and upper bound doses from intakes by inhalation or ingestion of the combined radionuclides in a mixture produced by alpha particles, or by beta particles plus gamma rays are given by:

$$D = \sum_{i=1}^n D_i \quad (10)$$

$$UB = \sum_{i=1}^n (UF_{int,i} D_i) \quad (11)$$

where

D	=	The total internal dose to a specific organ from all sources of intake (rem)
D_i	=	The i^{th} component internal dose to a specific organ (rem)
$UF_{int,i}$	=	The uncertainty factor for internal doses to a specific organ is assumed to be 10 in deterministic models except for incidental ingestion when the uncertainty factor is assumed to be 1
UB	=	The upper bound total internal dose to a specific organ (rem)

5.1.2.2 Additional Uncertainty in Internal Dose from Mission Film Badges with Periods of Coverage Exceeding One Day

When film badge readings from mission film badges are used to determine internal doses, the estimated total dose is determined in accordance with SM ID01. In addition, to the internal dose uncertainty described above, an additional uncertainty is added to the overall uncertainty. The additional mission film badge uncertainty is determined using the difference between the internal dose calculated assuming that the entire dose was received on the film badge issue date and the internal dose assuming the entire dose was received on the film badge return date. The mission film badge uncertainty is combined in quadrature such as in Equation 14 with other independent sources of internal dose.

The uncertainty of the internal dose determined from mission film badge results, the uncertainty of internal doses based upon reconstructed gamma doses, and the upper bound dose for combined internal doses are given by:

$$u_{FB} = D_1 - D_2 \quad (12)$$

$$u_i = D_i(UF_{int,i} - 1) \quad (13)$$

$$UB = D + \sqrt{u_{FB}^2 + \sum_{i=1}^n u_i^2} \quad (14)$$

where

u_{FB}	=	The additional uncertainty for an internal dose calculated using mission film badges that have different issue and return dates (rem)
D_1	=	The internal dose calculated using mission film badge readings assuming all of the dose was received in an 8-hour period on the date of film badge issue (rem)
D_2	=	The internal dose calculated using mission film badge readings assuming all of the dose was received in an 8-hour period on the date of film badge return (rem)
u_i	=	The uncertainty for an internal dose from the i^{th} intake (rem)
UB	=	The upper bound of combined internal doses (rem)

5.1.3 Uncertainties and Upper Bounds in Skin Dose

5.1.3.1 Skin Doses from External Sources (Gamma and Beta Shine)

The uncertainties in skin doses from external gamma and beta shine sources not in contact with the skin are generally assumed to be no greater than the uncertainty in the associated external gamma dose from such an external source. This is due, in part, to the fact that the beta-to-gamma ratios used to relate external gamma dose to beta dose were intended to be high-sided estimates. Thus, most beta shine skin doses are assigned the same uncertainty factor (UF_{ext}) as their associated gamma skin dose, unless otherwise indicated. (Barss and Weitz, 2006) Beta shine doses and their accompanying external gamma skin doses are assumed to be fully correlated, as are most doses from a single source exposure location (e.g., multiple disparate periods aboard the same ship are treated as if all of those individual doses are fully correlated.)

Skin doses may be calculated from reconstructed external gamma doses or film badge readings.

Total Dose, Uncertainty and Upper Bound for Reconstructed Gamma and Beta Shine Skin Dose

The skin dose for n reconstructed external gamma doses is based on the reconstructed gamma doses ($D_{\gamma,i}$). The estimated beta shine skin dose, total skin dose, the uncertainty of the total skin dose, and the upper bound of the total skin dose are given by:

$$D_{\beta,i} = D_{\gamma,i} R_{\beta\gamma} \quad (15)$$

$$D_{Skin,i} = (D_{\gamma,i} + D_{\beta,i}) \quad (16)$$

$$D_{Skin} = \sum_{i=1}^n D_{Skin,i} \quad (17)$$

$$u_{\beta\gamma,i} = D_{Skin,i}(UF_{ext} - 1) \quad (18)$$

$$UB_{Skin} = D_{Skin} + \sqrt{\sum_{i=1}^n u_{\beta\gamma,i}^2} \quad (19)$$

where

$D_{\gamma,i}$	=	The i^{th} component of the gamma skin dose (rem)
$D_{\beta,i}$	=	The i^{th} correlated corresponding component mean beta skin dose (rem)
$R_{\beta\gamma}$	=	The beta-gamma ratio used to convert reconstructed whole body external gamma doses to beta shine skin doses
$D_{Skin,i}$	=	The i^{th} component of combined beta and gamma skin dose (rem)
D_{Skin}	=	The total skin dose (rem)
$u_{\beta\gamma,i}$	=	The uncertainty associated with the i^{th} component of the beta plus gamma reconstructed skin doses (rem)
UB_{Skin}	=	The total upper bound skin dose (rem)

Note that it is possible to accrue a gamma skin dose without an accompanying beta shine dose, in which case the corresponding beta terms for that particular gamma dose are all zero.

5.1.3.2 Skin Doses Based on Film Badge Readings

Film badges were often worn in areas affected by fallout or neutron activation and measured the external gamma doses that resulted from exposures to these sources. The beta shine skin dose from accompanying beta radiation, while not directly recorded by

the film badge, can be correlated with the measured gamma dose by means of beta-to-gamma ratios. In such cases, the upper bound skin dose is calculated based on the upper bound of the film badge dose. The upper bound of a total beta dose that is based on multiple film badge readings can be calculated by multiplying the ratio of the total mean and total upper bound film badge doses by the total mean beta dose.

Reconstructed Gamma and Beta Skin Dose Combined with Film Badge-Derived Skin Dose

If a skin dose is estimated by reconstructed external gamma doses and film badge doses, the total skin dose and the upper bound of the skin dose are given by:

$$D_{Skin} = \sum_{i=1}^n (D_{Skin,i}) + FB_{\gamma}(1 + R_{\beta\gamma}) \quad (20)$$

$$u_{FB\beta\gamma} = (FB_{UB\gamma} - FB_{MEAN})(1 + R_{\beta\gamma}) \quad (21)$$

$$UB_{Skin} = \sum_{i=1}^n D_{Skin,i} + FB_{MEAN}(1 + R_{\beta\gamma}) + \sqrt{\sum_{i=1}^n u_{\beta\gamma,i}^2 + u_{FB\beta\gamma}^2} \quad (22)$$

where

$u_{FB\beta\gamma}$ = The uncertainty of the skin dose determined from film badge doses (rem)

The same formula can be used for the combined beta and gamma skin dose that is based only on film badge results by setting the other variables to zero.

5.1.3.3 Skin Contamination Dose

Skin contamination doses were not routinely reported prior to the NRC recommendations of 2003. Thus, a methodology (and accompanying uncertainty analysis) has been developed to address that need (SM ED04). The uncertainties in the doses associated with skin contamination range from a factor of 4 up to a maximum of slightly less than 18, depending on the location of the skin cancer site. (Apostoaie et al., 2005) All skin contamination doses can be assumed to be fully correlated. Though it is possible that there is some degree of independence among the component doses, NTPR assumes the component doses are fully correlated.

The total skin contamination dose is simply the sum of all the component skin contamination doses and the total upper bound skin contamination dose is the sum of all the component upper bound skin contamination doses. Each component of the skin contamination dose (descending and resuspended) has its own uncertainty. For n sources of skin contamination, the total skin contamination dose and the upper bound skin contamination dose are given by:

$$D_{SC} = \sum_{i=1}^n D_{SC,i} \quad (23)$$

$$UB_{SC} = \sum_{i=1}^n (UF_{SC,i} D_{SC,i}) \quad (24)$$

where

D_{SC}	=	Total skin contamination dose from all sources of contamination (rem)
$D_{SC,i}$	=	The i^{th} component skin contamination dose (rem)
$UF_{SC,i}$	=	Uncertainty factor associated with the i^{th} skin contamination dose (See SM ED04)
UB_{SC}	=	Upper bound total skin contamination dose (rem)

5.1.3.4 Combined Skin Dose

The total skin dose is the sum of the component skin doses. As with the external gamma doses, the dose distribution associated with each category of uncertainty is assumed to be normal. The uncertainties would be combined in quadrature and the upper bound would be the sum of the mean doses and the combined uncertainties.

5.2 Probabilistic Method

The alternative approach for treating uncertainties is the probabilistic or Monte Carlo method. In a Monte Carlo simulation, each input parameter is considered as a random variable whose value is determined by randomly sampling from its assigned probability distribution. These distributions reflect the variability and uncertainties in the values of the associated input parameters. The collection of sampled values, one per input parameter, defines a “scenario.” An output quantity, such as an external or internal dose, is then computed for each scenario using an algorithm that models the relevant physical and biological processes; this calculation constitutes one “history.” By repeating this procedure for many histories, a distribution of output values is accumulated. Analysis of the output distribution yields statistical parameters such as its mean, standard deviation, and percentiles, all of which increasingly represent their corresponding “true” population values as the number of histories increases. Monte Carlo methods can become

computationally intensive if the algorithm is complex and the number of histories is large.

As indicated, the probabilistic method requires that the uncertainties of input parameters be represented as probability distributions. However, not all input parameters require such formal representations. It is obviously unnecessary to develop uncertainty distributions for input parameters that have virtually no uncertainty – an arrival or departure date confirmed by ship’s logs, travel orders, flight manifests, morning reports and/or muster logs can be considered to have little or no uncertainty unless there are conflicts in such documentation. (The formal probability distributions in such cases are sharply-peaked delta functions.) Other input parameters, while uncertain, may have negligible impact on dose and likewise do not require the development of distributions—a participant’s arrival date at a test site may be uncertain, but this uncertainty is not important if it is known that he arrived before the first fallout event at a previously uncontaminated location. Thus, the first task in the application of the probabilistic method to dose reconstruction is to screen all input parameters to identify those which warrant the formal development of uncertainty distributions.

The next task is to develop or acquire the requisite parameter uncertainty distributions. Much of the remainder of this section and Attachment 2 are devoted to this topic. Once accomplished, the parameter distributions are input to a computer program which contains the Monte Carlo sampling logic. The program selects values of a parameter from its assigned distribution as it executes the iterative Monte Carlo algorithm to generate the output distributions of external and internal doses. A typical probabilistic dose reconstruction is based on 10,000 histories, each involving the random sampling of multiple input parameter distributions. The 95th percentiles of the output dose distributions, representing the doses accrued by at least 95 percent of the exposed population—personnel involved in similar activities—are taken as the respective upper bounds.

The following two subsections focus on uncertainty modeling of parameters associated with external and internal doses, respectively. The probabilistic methodology has not yet been extended to neutron doses and beta skin/eye doses.

5.2.1 Uncertainties in External Dose

Input parameters for external dose models may be categorized as operational parameters that define a participant’s location, movement, and habitat, and environmental parameters that characterize the radiation environment in his vicinity. The modeling of uncertainties for parameters of both types is discussed below.

5.2.1.1 Operational Parameters

Site Arrival/Departure Dates/Times

Dates of arrival and departure from test sites are generally well known. If an uncertainty exists in one of these dates that may impact the reconstructed doses, each of the candidate

dates may be assigned a probability that reflects the likelihood it is the correct date. For arrival date, in light of the remarks made above, this will be required for only if the participant arrived at a previously contaminated location and/or after the first fallout event. As examples, if it is known that a participant arrived at a test site no earlier than May 5 and no later than May 25, in the absence of any other information a uniform distribution covering the inclusive period May 5–25 can be used. If a morning report indicates that he departed on July 25 but travel orders list a departure date of July 28, and the documentation is considered equally authoritative, each of those dates could be assigned a probability of 0.5 and his departure date treated stochastically.

Arrival and departure times are usually less well known than the dates, but they generally have a proportionally smaller impact on reconstructed dose. Time may be important if a radiologically significant event, such as an abrupt, intense period of fallout, occurred on the day of arrival or departure, for which the participant may or may not have been present depending on the timing of his arrival or departure. In cases where the arrival/departure time may be important, that parameter can be modeled as uniform over some interval if all times within that interval are considered equally likely, or with a non-uniform distribution if some times are thought to be more likely than others.

Film Badge Issue/Return Dates/Times

There are frequently inconsistencies in film badge issue and/or return dates entered in the dosimetric record. As a common example, the dosimetry record of a participant issued a sequence of badges states that he turned in his first badge a number of days after receiving his second. If taken literally, this implies that he had two badges in the interim, whereas documented radiation safety procedures indicate that badge turn-in and receipt occurred concurrently. Apparent discrepancies of this type are usually resolved in deterministic assessments by assuming the actual turn-in date of the first badge coincides with the issue date of the second. While this may be a likely scenario, it is still possible that the dates in the dosimetry record are correct. In a probabilistic assessment, the turn-in date can be treated as a random variable to be selected on the basis of probabilities assigned to the two dates.

The time of a film badge exchange is usually unknown. In the unlikely event that this time impacts a dose reconstruction, it can be treated as a random variable in a manner similar to that discussed above regarding arrival and departure times.

Maneuver Characteristics

Maneuvers frequently were conducted at the Nevada Test Site (NTS) in conjunction with nuclear detonations. These events are characterized by parameters such as start times, march rates, distances of closest approach to radioactive objects or sites, and linger times at critical locations. The uncertainties of these and similar continuous parameters can be modeled using probability distribution functions (pdfs) of the forms discussed in Weitz et al. (2009). For example, the uncertainty in rate of march toward an objective can be

represented by a triangular distribution whose defining characteristics (minimum, most likely, and maximum march speeds) are assigned in consideration of the distance, known duration times, weather, and type of terrain traversed. Discrete probability distributions may also be relevant. If it is known that, of 1000 Marines who took part in a maneuver, 700 followed path A to an objective and 300 followed path B, the reasonable pdf for cases where this parameter is unknown would have two discrete outcomes: path A with probability 0.7 and path B with probability 0.3.

Fraction of Time Spent Outside

The fraction of time a participant spent outside versus inside while in a fallout field impacted his external dose because buildings and other structures provide partial shielding to the outside environment. Lacking specific statistical data on this parameter for an individual or a cohort, a triangular distribution is recommended. Factors such as the participant's job, the weather, the availability of outdoor recreational facilities, and veteran-provided information, are considered in assigning the distribution's defining values of minimum, most likely, and maximum fraction of time outdoors. Default values are provided in SM ED02.

Structural Occupancy

The types of structures a participant occupied while not outside impacted his dose because structures of different types provide varying degrees of protection from radiation (see discuss of structural shielding below). It was common for personnel stationed on one of the residence islands in the Pacific Proving Ground (PPG) to work in wood-framed buildings and billet in tents. If, while indoors, a participant spent the majority of his time in one or the other of these two structures, a relevant input parameter is the fraction of his indoor time he spent in a tent (versus in a building). If specific statistical information on this parameter for an individual or cohort is not available, a triangular distribution is recommended. Factors such as job responsibilities, shift hours, and building type are considered in assigning the distribution's defining values of minimum, most likely, and maximum fraction of time inside a tent. SM ED02 lists default values.

5.2.1.2 Environmental Parameters

Film Badge Results

The uncertainty in film badge exposure readings is modeled by a lognormal distribution (NRC, 1989, pp. 61–74), which defined two quantities—the measurement bias B and the 95th percentile uncertainty factor K . As the name implies, B is the estimated systematic error or bias introduced into the measurement process by, for example, an error in film calibration, pre-issue exposure of the film to radiation, or fogging of the film due to heat and/or humidity. K is a measure of the random error characterized by the lognormal distribution, and is related to the geometric standard deviation (GSD) by:

$$K = GSD^{1.645} \quad (25)$$

The usefulness of this parameterization lies in the fact that there is only a 5-percent probability that the true exposure associated with a film badge-measured exposure E —the film badge reading—is greater than $K \cdot E/B$. Estimates of B and K , by nuclear test series, are provided in NRC (1989). From these, the geometric mean $GM = E/B$ and $GSD = K^{1/1.645}$ are determined and the lognormal distribution representing the uncertainty in a film badge reading is thereby defined. The resulting distributions can be combined with the distributions for other dose components to produce an overall dose distribution and associated parameters (mean and upper bound).

Radiation Intensity Reading Data

The uncertainty in intensity reading data represents the overall error in intensity readings collected using survey meters or similar instruments, then processed and recorded in data logs and other documentation. These errors resulted mainly from inherent instrument precision, calibration error, instrument drift, operator bias, data processing tools, and data recording errors. On the basis of previous modeling efforts, it is recommended that the uncertainty in intensity reading data be modeled as a normal distribution with an uncertainty factor of 1.5 to 2, as indicated in Table 2. This uncertainty factor, defined as the ratio of the 95th percentile to the mean of the normally distributed intensity reading data, is a dimensionless quantity to be used as a multiplier on the estimated central value of the intensity reading data.

Use of Iso-Intensity Contour Maps

When using measurements or iso-intensity maps to estimate point values in time and space (location), the related uncertainty is comprised of two components. The first component is the uncertainty from errors in the intensity reading data (see source of uncertainty from radiation intensity reading data discussed above) and uncertainty introduced when maps are created from a discrete and often sparse set of point observation measurement data. The second component is the additional uncertainty that arises when an estimate is made at any point on a map by interpolation (or in some cases by extrapolation) from an iso-intensity contour map. In addition, when assessing the radiation environment for atmospheric nuclear test participants, information on the reliability of data collection and processing is often lacking and adds to the overall uncertainty from modeling the radiation environment.

The guidelines in Table 2 provide ranges of uncertainty factors and types of distributions that are based on the various sources of uncertainties and their cumulative effects (Chehata, 2009). The uncertainty factor, defined as the ratio of the 95th percentile to the central estimate of the variable distribution, is a dimensionless quantity to be used as a multiplier on the estimated central value of the radiation intensity. The selection of an uncertainty factor within the suggested ranges should be based on knowledge of the

reliability of the documentation and the methods used to produce the supporting iso-intensity map.

Non-Uniformity of Intensity

A model of the time-dependent, area-averaged outdoor intensity on each of the residence islands at PPG is well established for each fallout event. The outdoor intensity as a function of location on the island undoubtedly varied about this average, and at the locations occupied by a participant (e.g., at his work site, in his billet area, at a recreational area) may have been greater or less than the average. This uncertainty in the site-to-site variation in intensity on the residence islands is characterized with a lognormal distribution having a geometric mean of 1.0 and a geometric standard deviation of 1.5 as provided in SM ED02 and in Weitz et al. (2009).

For ships that received fallout from a nuclear test, the area-averaged topside intensity was frequently documented in deck logs, in operational reports, or an average intensity can reasonably be inferred from intensity readings reported on nearby ships or land masses. The variability of intensity with topside location contributes to the uncertainty in the external dose of an individual crewman who may have manned a topside workstation where the intensity differed significantly from the average. When calculating doses probabilistically the algorithm available in Weitz (2009a) is recommended for estimating the distributions of gamma intensities on the weather decks of fallout-contaminated ships with appropriate user-supplied values of the input parameters to generate ship-specific distributions of topside intensity.

Intensity Decay Rate

The radiation intensity in a fallout contaminated area will decrease with time due to radiological decay and weathering. As discussed in SM ID01 shot-specific, time-dependent radiological decay functions can be obtained directly from the FIIDOS software (Raine et al., 2007). The primary uncertainty in the FIIDOS-derived decay functions is the degree to which radiochemistry data based on cloud samples are representative of the radionuclide mix that was deposited and remained on the ground at any given location. That is, how much fractionation took place during the deposition process and thereafter due to weathering. Inherent in the FIIDOS database is the assumption that no fractionation, other than removal of noble gases, occurred during and after deposition. A rigorous study of fractionation has not yet been performed.

Lacking that, an empirical model of the uncertainty in decay rate was developed and is recommended for NTPR assessments. In that model, the FIIDOS decay functions are multiplied by a time-dependent error factor $(t/t_0)^a$, where exponent a is drawn from an appropriate normal distribution. Justification and details of this model are provided in Weitz et al. (2009). Parameters of the distribution for a are provided in SM ED02,.

Table 2. Proposed Ranges of Uncertainty Factors for Estimating Point Values Using Measured Intensities and Iso-Intensity Contour Maps

Source of Uncertainty	Uncertainty Factor ^(*)	Distribution	Note
Instrument precision, calibration and operator error (this is applicable when no interpolation is carried out, i.e., where a measurement was recorded at the location of interest)	1.5 - 2	Normal	Location and time known
With additional uncertainty due to contouring scatter point data	2 - 3 ^(†)	Lognormal/ triangular	Lognormal most adequate for intensity distributions around and not far away from GZ
With additional uncertainty due to using contour maps to determine point estimates by <u>interpolation</u> (factor is higher when location and time of measurements are unknown or inaccurate)	3 - 5 ^(†)	Lognormal/ triangular	Lognormal most adequate for intensity distributions around and not far away from GZ
Additional uncertainty due to using contour maps to determine point estimates by <u>extrapolation</u>	5 - 10 ^(†)	Lognormal/ triangular	Lognormal most adequate for intensity distributions around and not far away from GZ
Extrapolation with high uncertainty from all other sources and surrogate data are used	10 - 15 ^(‡)	Lognormal/ triangular	Lognormal most adequate for intensity distributions around and not far away from GZ

(*) The 95-percent uncertainty factor (UF) is the ratio of the 95th percentile to the central estimate of the distribution, which in most cases is the median, mean, or geometric mean (e.g., lognormal distributions).

(†) Combined uncertainty factors, which include instrument and operator error and all antecedent uncertainty sources.

(‡) When surrogate data are used, estimates are presumed to be made by extrapolation, e.g., as when using processed intensity data from a neighboring ship or island.

Structural Shielding

The protection factor PF of a land-based structure, such as a building or tent, is defined as the quotient of the free-field radiation intensity outside the structure and the free-field radiation intensity inside the structure. Thus, it is a measure of the radiological protection provided by that structure. When performing probabilistic dose reconstructions for land-based personnel, the uncertainty in PF is characterized using both the physical properties of that structure (e.g., its width, length, type of construction material) and on the random location within the structure where an individual can be positioned. The algorithm for developing structure-specific PF uncertainty distributions is provided in Weitz (2009b) and is recommended as general procedure.

The shielding factor SF for ships is defined as the ratio of intensity at some below-deck location to the average topside intensity above the head of the exposed individual. The shielding factor depends on the characteristics of the ship, i.e., maximum width (beam), length, number of decks, deck height, and decking thickness, and on one's position within the ship (which deck and location on that deck). Uncertainties or variability in all these parameters are reflected collectively in the uncertainty distribution of SF . The algorithm described in Weitz (2009c) is recommended to calculate ship- and deck-specific shielding factor distributions from contaminants deposited on weather deck surfaces.

Film Badge Conversion Factor

The film badge conversion factor (F_B) is the ratio of dose recorded on a properly worn film badge to free-in-air integrated intensity. This factor, which accounts for body shielding of the film badge to gamma radiation, has been assigned the deterministic values of 0.7 for the standing position in a planar fallout field and 1.0 for one facing the source of radiation (e.g., a contaminated aircraft during an examination). However, the uncertainty in this parameter is expected to be relatively small and to contribute negligibly to the overall uncertainty in dose. For this reason, uncertainty distributions for F_B have not yet been developed.

5.2.2 Uncertainties in Internal Dose Models

Internal doses from inhalation and ingestion intakes of fallout and of neutron-activated soil and dust are evaluated in probabilistic assessments with the equations given in SM ID01. The input parameters for these internal dose models may be categorized as environmental parameters that characterize the contaminant environment and biokinetic parameters that relate the contaminant environment to human intake and organ dose. Techniques for quantifying the uncertainties for parameters of both types are discussed below.

5.2.2.1 Contaminant Environment

Activity Fractions of Descending Fallout Particles

Internal dose from inhalation of descending fallout depends on the amount of activity fallout particles contain and the concentration in air of particles that can be inhaled. Particle size and activity are correlated, and as described in Weitz (2009d) these correlations are expressed as activity fractions. An activity fraction is defined as the fraction of total activity that is carried by particles with sizes within a specific range.

For probabilistic dose assessments, the activity fractions AF_1 , AF_2 , and AF_3 are calculated for the particle aerodynamic diameter in three size classes—1, 2, and 3. These activity fractions are calculated as described in SM ID01 using the parameters AF_{100} , f_1 and f_2 , where AF_{100} is the fraction of total activity carried by all particles with diameters less than 100 μm , and f_1 and f_2 are the fractions of AF_{100} that are attributable to particles in size Class 1 and Class 2, respectively.

For a given fallout event, values of the parameters AF_{100} , f_1 , and f_2 are randomly sampled from their assigned triangular distributions. A distribution for the fraction of AF_{100} that is attributable to particles in size Class 3 is generated using the quantity $(1 - f_1 - f_2)$. The distribution for AF_{100} is shot-specific, and those for f_1 and f_2 are generic. The minimum, most likely, and maximum values for these uncertainty distributions are provided in Weitz (2009d) and are summarized in SM ID01.

Deposition Velocity

Internal dose from inhalation of descending fallout is inversely related to the velocities at which fallout particles descend to the ground (deposition velocities), as seen in SM ID01. Three such velocities, V_1 , V_2 , and V_3 , one for each of the size classes specified above, have been modeled for use in probabilistic analyses. The uncertainty distributions assigned to these deposition velocities are log-triangular with the parameters given in Weitz (2009e) and in SM ID01.

Gamma Source Modification Factor

Ratios of surface activity density to intensity (Ci m^{-2} per R hr^{-1}), generated with the FIIDOS code for infinite plane sources, are used in internal dose calculations to estimate airborne activity concentrations based on intensity measurements. The Gamma Source Modification Factor ($GSMF$) corrects for the fact that the contaminated surface was not infinite in spatial extent, as assumed in the FIIDOS calculations. For land-based applications, the area of fallout deposition was generally large enough that the correction is insignificant. Thus, for exposures to fallout on land, $GSMF$ is set equal to 1.

However, for shipboard exposure scenarios, the contaminated area was limited to the weather deck of the ship and the correction is necessary. Weitz (2009e) discusses the formulation of $GSMF$ for probabilistic assessments of shipboard exposures and provides

Mathcad-based programs for generating ship-specific distributions for aircraft carriers, ships with elliptical shapes and superstructure.

Activity Density-to-Intensity (FIIDOS) Ratios

The discussion above on *GSMF* focuses on how to adjust the value of the FIIDOS-generated surface activity density-to-intensity ratios to account for finite source size. There is an underlying uncertainty in the FIIDOS ratios themselves, independent of source size. A major contributor to this uncertainty is fractionation, which has not yet been taken into account. Quantification of this uncertainty is a subject for future study.

Resuspension Factor

The resuspension factor K (m^{-1}), defined as the ratio of air activity concentration in Ci m^{-3} to surface activity density in Ci m^{-2} , is an important input parameter in the calculations of internal dose from resuspended fallout (SM ID01). For a probabilistic analysis, the time-dependent expression given in SM ID01 is used for resuspension due to typical land-based activities. It is recommended that the uncertainty associated with this parameter be estimated for each history by multiplying each calculated value of K by a factor randomly selected from a lognormal distribution with a geometric mean of 1.0 and a geometric standard deviation of 4.05. This distribution, discussed in Weitz et al. (2009) is based on the results of a study reported in Anspaugh et al. (2002).

For blast-driven resuspension of fallout, different resuspension factors are based upon a non-time dependent value of K with a log-normal distribution that depend on proximity to the blast and the size of the blast. The blast-driven resuspension of fallout resuspension factors for the blast-wave region and the thermal-pulse (formerly precursor) region can be found in SM ID01.

5.2.2.2 Biokinetic Parameters

Breathing Rate

Physiological parameters related to ventilation influence the volume and rate of air inhaled and the proportions entering through the nose and mouth, thus affecting the amount of radioactive particles and gases inhaled, their penetration into the respiratory tract, and the quantities deposited.

Breathing characteristics and respiratory parameters vary among individuals because they are largely a function of age and body size, level of physical activity, state of health of the respiratory tract, and if the individual is a smoker. The distribution of breathing rates appropriate for nuclear test participants developed in Weitz et al. (2009), is recommended for performing probabilistic analyses of internal dose. This distribution is triangular with the defining values of minimum, most likely, and maximum breathing rates given in SM ID01.

Respiratory Tract Deposition Fractions

Respiratory tract deposition fractions are defined as the fractions of inhaled particles in a given size class that deposit in a defined portion of the human respiratory tract. For use in the NTPR probabilistic methodology, deposition fractions for two regions are defined, the posterior extra-thoracic (ET₂) region and thoracic (TH) airway (bronchial, bronchiolar, and alveolar-interstitial regions). Particles are described by the same classes—1, 2, and 3—as those for activity fractions. Characterizations of deposition fractions of particle size classes for use as modifying factors are described in SM ID01 and are designated in Mathcad implementations as R_1 , R_2 , and R_3 for particles that deposit in the thoracic region, and as NR_1 , NR_2 , and NR_3 for particles that deposit in ET₂. These characterizations are derived in McKenzie-Carter and Stiver (2009). The values and distributions of these modifying factors, are provided in SM ID01. These multiplicative parameters are used only in descending fallout scenarios (SM ID01).

Dose Conversion Factors

Dose conversion factors (*DCF*s) are used in NTPR dose reconstructions for the assessment of doses accrued from internally-deposited radionuclides by the inhalation and ingestion pathways. Specific applications to the reconstruction of internal doses resulting from the inhalation of resuspended and descending fallout are given in SM ID01.

The uncertainties in inhalation and ingestion *DCF*s are incorporated into the NTPR modeling by multiplying the unbiased *DCF*s—discussed in SM ID01—by lognormal distributions. For these lognormal distributions, the geometric means are set equal to 1.0 and the geometric standard deviations are assigned such that the ratios of the 95th percentiles to their geometric means are 30 (equivalent to $GSD = 7.91$) for alpha *DCF*s and 10 ($GSD = 4.05$) for beta-plus-gamma *DCF*s (Weitz et al.; 2009; Kocher et al, 2009). These parameters are also provided in SM ID01.

Incidental Ingestion

A pathway considered in the case studies of land-based units is incidental ingestion, a chronic type of exposure that involves the daily intake of relatively small quantities of contaminated soil and dust. The sources of the ingested contamination include direct contact with airborne soil and dust due to walking, vehicular traffic, and wind-driven lofting of contaminated particles in areas where military personnel were temporarily stationed. Routine daily activities by test participants may also have involved the inadvertent ingestion of small quantities of soil and dust particles that adhered to food, beverages, cigarettes, or their hands.

SM ID01 contains the equation describing the basis for probabilistic assessments of internal dose from incidental ingestion. Uncertainty models for most of the parameters

appearing in that equation (e.g., intensity, DCF_{ing}) have been addressed in Weitz et al. (2009). There are two parameters specific to this pathway, however, whose uncertainties are additionally modeled. These parameters are q_{ing} , the soil ingestion rate, and ρ_{soil} , the bulk density of the soil. It is recommended that the uncertainties of both these quantities be modeled with triangular distributions, the characteristics of which are developed in Chehata and Stiver (2009) and tabulated in SM ID01.

5.2.3 Treatment of Correlations

Potential correlations among uncertainties of key parameters must be considered in formulating the Monte Carlo sampling of parameter values from their assigned pdfs. The degree of correlation between two parameters can range continuously from none (their values are completely independent) to full (the value of one is entirely predictable based on the value of the other). Nevertheless, correlations between parameters in NTPR probabilistic assessments have been assumed to be either non-existent or full; methods of modeling partial correlations have not yet been integrated into the probabilistic formalism. Correlations are addressed much more fully in Appendix G of Weitz et al. (2009).

In performing probabilistic analyses of internal dose accrual, it is recommended that uncertainty distributions that are uncorrelated be sampled independently by drawing separate random numbers during each history. It is further recommended that fully correlated distributions be sampled using the same random number.

6 Data and Input

Operation and shot-specific data are compiled in Appendices A–C. Attachment 1 to this SM provides sample uncertainty calculations. Attachment 2 provides guidance on the implementation of the pdfs described in Weitz et al. (2009) used in probabilistic dose calculations.

7 Referenced SOPs from this Manual

- (1) SOP RA01 - Radiation Dose Assessment for Cases Requiring Detailed Analysis
- (2) SM ED01 - Film Badge Dose Assessment
- (3) SM ED02 - Whole Body External Dose - Reconstruction
- (4) SM ID01 - Doses to Organs from Intake of Radioactive Materials

8 Reference Materials

- (1) Anspaugh, L.R., Simon, S.L., Gordeev, K.I., Likhtarev, I.A., Maxwell, R.M., and Shinkarev, S.M., 2002. Movement of Radionuclides in Terrestrial Ecosystems by Physical Processes. *Health Physics* 82:669–679.

- (2) Apostoaei, A. Iulian and Kocher, David C., 2005. Skin Doses from Dermal Contamination. Draft Report to the Defense Threat Reduction Agency. (SENES Oak Ridge, Inc. Oak Ridge, TN) (September).
- (3) Barss, Neil M. and Weitz, Ronald L., 2006. Reconstruction of External Dose from Beta Radiation Sources of Nuclear Weapon Origin. *Health Physics* 91:379–389.
- (4) Chehata, M., 2009. *Uncertainty in Estimating Radiation Intensity from Intensity Measurements and Iso-Intensity Maps*. NTPR-TM-09-13, Science Applications International Corporation, McLean, VA.
- (5) Chehata, M., and Stiver, J., 2009. *Evaluation of Internal Doses from Incidental Ingestion of Contaminated Soil and Dust for NTPR Participants at the Nevada Test Site and Pacific Residence Islands*. NTPR-TM-09-03, Science Applications International Corporation, McLean, VA.
- (6) DTRA (Defense Threat Reduction Agency), 2003. “DTRA01-01-C-0007 (NTPR Interim Guidance from the Contracting Officer),” Letter: Defense Threat Reduction Agency to Titan Corporation (July 16).
- (7) DTRA (Defense Threat Reduction Agency), 2007. Policy and Guidance Manual - Nuclear Test Personnel Review Program, Revision 7, (Fort Belvoir, VA) (November 26).
- (8) Kocher, D., 2004. “Policy Statements To Implement Interim Guidance, SENES Oak Ridge, Inc., Oak Ridge, Tennessee (May 14).
- (9) Kocher, D.C., Trabalka, J.R., and Apostoaei, A.I., 2009. *Derivation of Effective Resuspension Factors in Scenarios for Inhalation Exposure Involving Resuspension of Previously-Deposited Fallout by Nuclear Detonations at Nevada Test Site*. DTRA-TR-09-15 (SENES Oak Ridge, Inc., Oak Ridge, TN and Defense Threat Reduction Agency, Fort Belvoir, VA).
- (10) McKenzie-Carter, M. and Stiver, J., 2009. *Deposition Fraction Modifications for Inhalation of Descending Fallout*. NTPR-TM-09-09, Science Applications International Corporation, McLean, VA.
- (11) NRC (National Research Council), 1989. *Film Badge Dosimetry in Atmospheric Nuclear Tests*, National Academy Press, Washington, DC.
- (12) NRC (National Research Council), 2003. *A Review of the Dose Reconstruction Program of the Defense Threat Reduction Agency*, National Academies Press, Washington, DC.
- (13) Raine, D.A. III, Egbert, S.D., Stiver, J.H., and Case, D.R., 2007. *FIIDOS—A Computer Code for the Computation of Fallout Inhalation and Ingestion Dose to Organs, Computer User’s Guide (Revision 4)*. DTRA-TR-07-11, Science Applications International Corporation, McLean, VA and Defense Threat Reduction Agency, Fort Belvoir, VA.
- (14) SAIC (Science Applications International Corporation), 2006. FBDOSE User’s Guide, Science Applications International Corporation, McLean, VA (June 26).

- (15) USNRC (U.S. Nuclear Regulatory Commission), 2006. Standards for Protection Against Radiation, Title 10, Code of Federal Regulations, Part 20.
- (16) Weitz, R.L., 2009a. *Development of a Topside Intensity Distribution Model*. NTPR-TM-09-05, Science Applications International Corporation, McLean, VA.
- (17) Weitz, R.L., 2009b. *Protection Factors for Land-Based Structures*. NTPR-TM-09-10, Science Applications International Corporation, McLean, VA.
- (18) Weitz, R.L., 2009c. *Shielding Factors for Ships*. NTPR-TM-09-11, Science Applications International Corporation, McLean, VA.
- (19) Weitz, R.L., 2009d. *Characterization of Descending Fallout*. NTPR-TM-09-06, Science Applications International Corporation, McLean, VA.
- (20) Weitz, R.L., 2009e. *Gamma Source Modification Factor*. NTPR-TM-09-04, Science Applications International Corporation, McLean, VA.
- (21) Weitz, R.L., Case, D. R., Chehata, M., Egbert, S. D., Mason, C. L., Singer, H. A., Martinez, D. G.; McKenzie-Carter, M. A.; and Stiver, J. S., 2009. *Probabilistic Approach to Uncertainty Analysis in NTPR Radiation Dose Assessments*. DTRA-TR-09-13 (Science Applications International Corporation, McLean, VA and Defense Threat Reduction Agency, Fort Belvoir, VA).
- (22) Weitz, R.L., and Egbert, S.D., 2009. *Compilation of Initial Radiation Doses to Atmospheric Test Participants*. NTPR-TM-09-01, Science Applications International Corporation, McLean, VA.

Attachment 1 Sample Uncertainty Calculations

The following sections contain calculations and clarifying explanations detailing how to calculate the total upper bound doses in various situations.

A1-1 Sample Calculations for External Gamma Doses

a. Independent Reconstructed Gamma Doses

This example is for two reconstructed external gamma doses, a reconstructed dose $D_{\gamma,1}$ of 1.000 rem and a reconstructed dose $D_{\gamma,2}$ of 0.1 rem. The uncertainty for $D_{\gamma,1}$ ($u_{\gamma,1}$) is 2 rem from $D_{\gamma,1} \times (UF_{ext} - 1)$ ($1.0 \times (3 - 1)$). The uncertainty for $D_{\gamma,2}$ ($u_{\gamma,2}$) is 0.2 rem from $D_{\gamma,2} \times (UF_{ext} - 1)$ ($0.1 \times (3 - 1)$). The uncertainty is calculated using Equation 3 above.

The total reconstructed external gamma dose (D_{γ}) is 1.1 rem from $D_{\gamma,1} + D_{\gamma,2}$ ($1.0 + 0.1$). The upper bound for the total estimate gamma dose is then 3.109 from $D_{\gamma,1} + D_{\gamma,2}$ plus the square root of $(u_{\gamma,1}^2 + u_{\gamma,2}^2)$ ($1.0 \text{ rem} + 0.1 \text{ rem} + 2.01 \text{ rem}$). Note: 2.01 rem is from the square root of $((2.0)^2 + (0.2)^2)$. The total dose is calculated using Equation 2 above. The upper bound dose is calculated using Equation 4 above.

b. A Reconstructed Gamma Dose and a Film Badge Dose

This example is for a reconstructed external gamma dose ($D_{\gamma,1}$) of 1.0 rem and a film badge dose using the data from the FBDOSE output in Table 1. The total estimated whole body external gamma dose (D_{γ}) is 2.390 rem from $D_{\gamma,1} + FB_{\gamma}$ ($1.0 \text{ rem} + 1.390 \text{ rem}$), where FB_{γ} (1.390 rem) is the total from the MRAJD column in the FBDOSE output. The total dose is calculated using Equation 8.

The uncertainty for $D_{\gamma,1}$ ($u_{\gamma,1}$) is 2.0 rem from $D_{\gamma,1} \times (UF_{ext} - 1)$ ($1.0 \text{ rem} \times (3 - 1)$). The uncertainty of the film badge dose FB_{γ} ($u_{FB\gamma}$) is 0.342 rem from $FB_{UB} - FB_{MEAN}$ (the total of the UPP90 column from the FBDOSE output minus the total of the MEAN column of the FBDOSE output) ($1.557 \text{ rem} - 1.215 \text{ rem}$). The upper bound for the total estimated gamma dose is 4.244 rem from $D_{\gamma,1} + FB_{MEAN}$ + the square root of $(u_{\gamma,1}^2 + u_{FB\gamma}^2)$ ($1.0 \text{ rem} + 1.215 \text{ rem} + 2.029 \text{ rem}$). Note: 1.215 rem is from the total of the MEAN column in the FBDOSE output and 2.029 rem is from the square root of $((2.0 \text{ rem})^2 + (0.342 \text{ rem})^2)$. The uncertainty for the film badge dose is calculated using Equation 7. The upper bound of the total dose is calculated using Equation 9.

A1-2 Sample Calculation for Total Internal Dose

This example is for two internal doses to the same organ, reconstructed beta-gamma dose resuspended fallout (D_1) of 1.000 rem and an incidental ingestion dose D_2 of 0.1 rem.

Note that the method does not change with additional internal doses, there are just more terms.

The total internal dose (D) is 1.1 rem from $D_1 + D_2$ (1 rem + 0.1 rem). The upper bound for the internal dose for a single organ is 10.1 rem from $(UF_{int,1} \times D_1 + UF_{int,2} \times D_2)$ (10×1 rem + 1×0.1 rem). The total dose is calculated using Equation 10 and the upper bound dose is calculated using Equation 11.

A1-3 Sample Calculation for Total Skin Contamination Dose

This example is for two independent skin contamination doses, skin contamination dose $D_{SC,1}$ of 2.0 rem and a skin dose $D_{SC,2}$ of 0.2 rem. The uncertainty factors $UF_{SC,1}$ and $UF_{SC,2}$ are assumed to be the same for both doses and are 11 for this example. The uncertainty factors are determined as part of the original skin contamination dose (See SM ED 04).

The total skin contamination dose (D_{sc}) is 2.2 rem from $D_{SC,1} + D_{SC,2}$ (2.0 rem + 0.2 rem). The upper bound dose (UB_{SC}) is 24.2 rem from $D_{SC,1} \times UF_{SC,1} + D_{SC,2} \times UF_{SC,2}$ (2.0 rem \times 11 + 0.2 rem \times 11). The total skin contamination dose is calculated using Equation 22 and the upper bound for the skin contamination dose is calculated using Equation 23.

A1-4 Sample Calculation for Total Skin Dose from External Sources

a. Independent Reconstructed Gamma and Beta Skin Doses

This example is for two reconstructed external gamma skin doses and two beta doses that are correlated with the external gamma skin doses. One reconstructed gamma skin dose ($D_{\gamma,1}$) is 0.3 rem. Assuming a beta-gamma ratio ($R_{\beta\gamma}$) of 7.33, the correlated beta skin dose ($D_{\beta,1}$) is 2.2 rem from $D_{\gamma,1} \times R_{\beta\gamma}$ (0.3×7.33). The second reconstructed gamma dose ($D_{\gamma,2}$) is 0.1 rem. Assuming the same beta-gamma ratio, the beta skin dose ($D_{\beta,2}$) is 0.733 rem from $D_{\gamma,2} \times R_{\beta\gamma}$ (0.1×7.33). The uncertainty for $D_{Skin,1}$ ($u_{\beta\gamma,1}$) is 5 rem from $(D_{\gamma,1} + D_{\beta,1}) \times (UF_{ext} - 1)$ ($(0.3 + 2.2) \times (3 - 1)$). The uncertainty for $D_{Skin,2}$ ($u_{\beta\gamma,2}$) is 1.66 rem from $(D_{\gamma,2} + D_{\beta,2}) \times (UF_{ext} - 1)$ ($(0.1 + 0.733) \times (3 - 1)$). The beta shine skin dose is calculated using Equation 15. The total skin dose from gamma and beta shine from a single source is calculated using Equation 16. The uncertainty for reconstructed skin dose from a single source is calculated using Equation 18.

The total gamma and beta shine skin dose is 3.33 rem from $D_{\gamma,1} + D_{\beta,1} + D_{\gamma,2} + D_{\beta,2}$ (0.3 rem + 2.2 rem + 0.1 rem + 0.73 rem). The upper bound dose is 8.60 rem from D_{skin} + the square root of $((u_{\beta\gamma,1})^2 + (u_{\beta\gamma,2})^2)$ (3.33 rem + 5.27 rem) where the square root of $((0.6$ rem + 4.4 rem)² + (0.2 rem + 1.46 rem)² is 5.27 rem.

b. A Reconstructed Gamma and Beta Dose and a Film Badge Dosimeter with a Corresponding Beta Dose

This example is for a simplified total skin dose using a reconstructed whole body external gamma dose ($D_{\gamma,1}$) of 0.3 rem and the sample FBDOSE output in Table 1. Assuming a beta-gamma ratio ($R_{\beta\gamma}$) of 7.33, the correlated beta skin dose ($D_{\beta,1}$) is 2.2 rem from $D_{\gamma,1} \times R_{\beta\gamma}$ (0.3×7.33). The total skin dose from the reconstructed skin dose is 2.5 rem from $D_{\gamma,1} + D_{\beta,1}$ ($0.3 + 2.2$). The uncertainty of the total reconstructed skin dose $D_{skin,1}$ ($u_{\beta\gamma,1}$) is 5.0 rem from $((D_{\gamma,1} + D_{\beta,1}) \times (UF_{ext} - 1))$ ($2.5 \text{ rem} \times (3 - 1)$).

The FB_{γ} is 1.390 rem and is taken from the total of the MRADJ column of the FBDOSE output in Table 1. The FB_{MEAN} is 1.217 rem and is taken from the total of the MEAN column of the FBDOSE output in Table 1. The $FB_{UB\gamma}$ is 1.557 rem and is taken from the total of the UPP90 column of the FBDOSE output in Table 1. The uncertainty of the total skin dose determined from film badge doses $u_{FB\beta\gamma}$ is 2.849 rem from $(FB_{UB\gamma} - FB_{MEAN}) \times (1 + R_{\beta\gamma})$ ($(1.557 - 1.217) \times (1 + 7.33)$). The uncertainty for the total skin dose from the film badge readings is calculated using Equation 21.

The total skin dose from gamma and beta dose from both the reconstructed external gamma dose and the film badge dose is 14.079 from $D_{skin,1} + FB_{\gamma} \times (1 + R_{\beta\gamma})$ ($0.3 + 2.2 + 1.390 \times (1 + 7.33)$). The upper bound for the total skin dose is 18.39 rem from $D_{skin,1} + FB_{MEAN} \times (1 + R_{\beta\gamma}) + \text{square root of } ((u_{\beta\gamma,1})^2 + (u_{FB\beta\gamma})^2)$ ($2.5 \text{ rem} + 1.217 \times (7.33 + 1) + 5.75$) where the square root of $((5 \text{ rem})^2 + (2.849)^2)$ is 5.75. The total skin dose is calculated using Equation 20. The upper bound skin dose is calculated using Equation 22.

Attachment 2 Implementation of Probability Density Functions in Mathcad

Mathcad is the platform most likely to be used for probabilistic dose reconstructions. For that reason, the implementation in Mathcad of specific and arbitrary probability density functions is outlined in this attachment.

Mathcad has a rather large array of pdfs in its internal library, including uniform, Gaussian, and lognormal. Hence, sampling from these pdfs can be readily implemented using the following standard Mathcad commands.

- $R_i = \text{runif}(n, a, b)_i$ – produces n values of a random variable R uniformly distributed between a and b .
- $R_i = \text{rnorm}(n, \mu, \sigma)_i$ – produces n values of a random variable R normally distributed with mean μ and standard deviation σ .
- $R_i = \text{rlnorm}(n, \ln(GM), \ln(GSD))_i$ – produces n values of a random variable R lognormally distributed with geometric mean GM and geometric standard deviation GSD .

There is a straightforward way of sampling from a pdf that are not in the Mathcad library, such as the triangular distribution. Let x be the variable of interest (e.g., a time duration, intensity reading, shielding factor) and $P(x)$ the pdf that characterizes the uncertainty in x . The cumulative probability function $C(x)$ is defined as:

$$C(x) = \int_{-\infty}^x P(x') dx' \quad (\text{A2-1})$$

The following algorithm allows one to sample x from an arbitrary pdf $P(x)$:

1. Perform the integration indicated in Equation A2-1, either in closed form or numerically, and set the resulting expression equal to a constant R , i.e., $C(x) = R$.
2. Solve this expression for x as a function of R , giving $x = f(R)$.
3. Sample R from a uniform random distribution between 0 and 1. This sampling can be accomplished using the Mathcad command for uniform distribution given above.
4. The resulting $x_i = f(R_i)$ will be distributed according to $P(x)$.

As an example of the use of this algorithm when $P(x)$ is expressed in a functional form that allows closed-form integration of Equation A2-1, consider a triangular distribution defined by $P(a) = 0$, $P(m) = P_k$ (peak value), and $P(b) = 0$, where $a \leq m \leq b$. The constraint that $C(\infty) = 1$ requires that $P_k = 2/(b-a)$. (Alternatively, this can be derived without formally integrating $C(x)$ by noting that the total area under $P(x)$ is $\frac{1}{2} \cdot P_k \cdot (b-a)$.) $P(x)$ can then be written in functional form as:

$$P(x) = \begin{cases} \frac{2(x-a)}{(m-a)(b-a)} & \text{for } a \leq x \leq m \\ \frac{2(b-x)}{(b-m)(b-a)} & \text{for } m < x \leq b \end{cases} \quad (\text{A2-2})$$

Substituting Equation A2-2 into Equation A2-1 and integrating gives:

$$C(x) = \begin{cases} \frac{(x-a)^2}{(m-a)(b-a)} & \text{for } a \leq x \leq m \\ \frac{m-a}{b-a} + \frac{(x-m)}{(b-m)(b-a)}(2b-m-x) & \text{for } m < x \leq b \end{cases} \quad (\text{A2-3})$$

Setting each of the two components of $C(x)$ in Equation A2-3 equal to R and solving the quadratic equations for x yields the desired result:

$$x = \begin{cases} a + \sqrt{R(m-a)(b-a)} & \text{for } 0 \leq R \leq (m-a)/(b-a) \\ b - \sqrt{(1-R)(b-m)(b-a)} & \text{for } (m-a)/(b-a) < R \leq 1 \end{cases} \quad (\text{A2-4})$$